

1 Q. Has Hydro identified any LIL failure conditions that could result in a blackout of the
2 IIS? In this response state whether an assessment of such a risk been performed for
3 all conceivable system states prior to a failure of the LIL.

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6 A. To date, Hydro's analysis and subsequent design for the integration of the LIL has
7 been based upon single contingency analysis assuming all equipment in service.
8 There has been no identified single contingency loss of the LIL components (i.e.
9 single element such as pole, transformer, valve, electrode conductor, etc.) that
10 results in a complete blackout or even partial load loss on the Island Interconnected
11 System. This approach is consistent with Hydro's past transmission planning
12 practices. Hydro believes this is consistent with the NERC TPL-001-4 standard
13 categories P0 and P1 (previously NERC TPL-001 and TPL-002). Further, Hydro's
14 analyses has considered peak, intermediate and light load cases. This approach is
15 consistent with the NPCC Directory #1 – Design and Operation of the Bulk Power
16 System December 1, 2009 which states at page 8:

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18 *Design studies shall assume **power** flow conditions utilizing*
19 *transfers, **load** and generation conditions which stress the system.*
20 *Transfer capability studies shall be based on the **load** and*
21 *generation conditions expected to exist for the period under study.*
22 *All **reclosing** facilities shall be assumed in service unless it is known*
23 *that such facilities will be rendered inoperative.*

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25 With respect to the Island Interconnected System, winter peak load conditions are
26 assessed as these conditions stress the system with respect to high power transfers
27 and corresponding low bus voltages and large electrical angles across the power

1 system. Intermediate loading conditions of spring and fall are considered as the
2 loading conditions exhibit impacts on the thermal loading of transmission lines. The
3 summer light load conditions are assessed as the condition tends to stress the
4 system with respect to high bus voltages and synchronous machines operating in
5 under excited mode, which is inherently dynamically less stable than the over
6 excited mode.

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8 Following the loss of a single element, the reliability criteria permit system
9 adjustment before loss of a second element. This analysis would be considered an
10 N-1 starting point and the contingencies then N-1-1 or P6 Multiple Contingency
11 (two overlapping singles) from NERC TPL-001-4. NERC requires system stability for
12 the event but permits interruption of firm transmissions service and non-
13 consequential load loss.

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15 It is Hydro's intent to consider the N-1-1 contingency analysis as part of the
16 operational studies. The approach is consistent with that prescribed in both the
17 NERC TPL standards and NPCC Directory #1. The outcome of the analysis will result
18 in operating procedures and necessary adjustment to protection schemes such as
19 the Under Frequency Load Shedding program which will prevent an Island wide
20 black out for the N-1-1 events. To this end an Island Wide Blackout is highly
21 improbable if all equipment operates in accordance with design and the system
22 operator follows standard operating procedures to keep line flows and voltages
23 within design limits. Hydro will not be completing an analysis for all conceivable
24 system states prior to the failure of the LIL. Given the number of system elements
25 and the range of system load the resultant combinations resulting in separate
26 system states would make the analysis impracticable. Given the nature of
27 interconnected transmission systems and the experience of many transmission

- 1 planners, the transmission planning processes and standards have been set to use
- 2 load and generation conditions expected during the study and load and generation
- 3 conditions that are known to stress the system as noted above.