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| 1  | Q. | Reference: CAN/CSA-C22.3 No. 60826-10, Design Criteria of Overhead Transmission       |
|----|----|---|
| 2  |    | Lines   |
| 3  |    | The referenced standard CAN/CSA-C22.3 No. 60826-10 states in Section 6.4.4.1 on       |
| 4  |    | page 73:  |
| 5  |    | "Wind velocities associated with icing episodes can be calculated from data, if       |
| 6  |    | available or, when there is little or no data, from the following assumptions. In the |
| 7  |    | latter case, the reference wind speed is multiplied by a reduction factor $B_i$ [0.4- |
| 8  |    | 0.5]"   |
| 9  |    | The response to Request for Information NP-NLH-004 indicates that a reduction         |
| 10 |    | factor of 0.4 was used to determine ice loading for the combined wind and ice         |
| 11 |    | loading criteria for the Labrador Island Link. Why has the minimum of the range       |
| 12 |    | (0.4 to 0.5) been selected? In your response, please indicate how Hydro               |
| 13 |    | incorporated Exhibit 95 - Evaluation of in-cloud icing in the Long Range Mountain     |
| 14 |    | Ridge from the Muskrat Falls Review which implies on page 50 of 96 that a factor of   |
| 15 |    | 0.5 is more appropriate.  |
| 16 |    |   |
| 17 |    |   |
| 18 | Α. | The analysis was undertaken to demonstrate that the Labrador-Island Transmission      |
| 19 |    | Link structures were capable of withstanding combined loads within the range as       |
| 20 |    | proposed by the standard, and the selected reduction factor is within the range as    |
| 21 |    | stated in the standard.   |
| 22 |    |   |
| 23 |    | The statement from Exhibit 95 does not offer additional guidance over the             |
| 24 |    | standard, noting that " it [the wind] may be around 50% of the maximum wind           |
| 25 |    | load with the same return period."  |
| 26 |    |   |
| 27 |    | Furthermore, the maximum structure utilization in the rime areas is less than 70%.    |